Soil desiccation cracks as a suction–contraction process

J. A. CORDERO*, G. USECHE*, P. C. PRAT*, A. LEDESSMA* and J. C. SANTAMARINA*

Recent macro- and particle-scale advances in unsaturated soil behaviour have led to an enhanced understanding of the effects of moisture changes on soil response. This research examines desiccation cracks as a suction–contraction-coupled process using sand–clay mixtures. Suction–moisture measurements highlight the role of fines on suction potential even at low fines content; on the other hand, oedometer tests exhibit a marked transition from sand-controlled to clay-controlled compressibility. Time-lapse photography of desiccation tests in flat trays show the onset of crack initiation and the subsequent evolution in horizontal strains; concurrent gravimetric water content measurements relate crack nucleation to suction at air entry. Suction and compressibility increase with the soil-specific surface and have a compounded effect on desiccation-driven lateral contraction. Both layer thickness and its lateral extent affect the development of desiccation cracks. The recently proposed revised soil classification system properly anticipates the transitions in compressibility and capillary phenomena observed in this study (between 15 and 35% fines content).

KEYWORDS: clays; compressibility; sands; suction

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INTRODUCTION

Soil desiccation is central to soil–atmosphere interaction. Eventually, desiccation-induced shrinkage may lead to the typical polygonal network of cracks that have been observed at different scales (Corte & Higashi, 1964; Hueckel et al., 2014). Soil properties, environmental characteristics and mechanical boundary conditions influence the evolution of desiccation cracks and patterns (Shokri et al., 2015).

Desiccation cracks alter the thermal, hydraulic and mechanical properties of soils (Vallejo, 2009). Crack formation is most relevant in the context of mine waste (Morris et al., 1992; Rodríguez et al., 2007), landfill liners, slope degradation, embankments, shallow foundations (Lozada et al., 2015), roads, agricultural lands (Sinnathamby et al., 2014), and even of the Martian landscape (El-Maarry et al., 2012).

Fundamentally, desiccation cracks are about changes in effective stress and volume contraction at the macroscale, and interparticle skeletal and capillary forces and grain displacements at the microscale. Desiccation cracks in soils are part of an extended family of open-mode discontinuities that include hydraulic fracturing, gas-driven fractures, ice or hydrate lenses, and even root growth (Shin & Santamarina, 2011a). Crack formation is intimately involved in fracture formation. Within this framework, the authors investigate the formation of desiccation cracks in soils as a coupled suction–contraction process.

CHARACTERISATION TESTS

The experimental study centres on 11 sand–kaolinite mixtures prepared in the following kaolinite mass fractions: $F_k = M_k/(M_k + M_s)$. 0, 5, 10, 15, 20, 25, 30, 40, 60, 80 and 100%. Table 1 summarises the individual material properties of the sand and kaolinite used in all mixtures. Experiments measured oedometric compressibility, suction against water content [soil water retention curves (SWRC)] and desiccation tests inside an environmental chamber at constant relative humidity RH and temperature $T$ for all mixtures. Characterisation tests are described next.

Compressibility

The 11 mixtures were tested in floating ring oedometers (internal diameter = 63.5 mm) to determine their compressibility between 1 and 1707 kPa. The saturated mixtures were prepared near the liquid limit (similar to subsequent desiccation tests). Stress-strain trends in Fig. 1 highlight the increased compressibility of the more plastic mixtures with kaolinite content.

Compression and recompression indices measured in oedometric tests show three marked zones (Fig. 2): mixtures with sand-controlled stiffness, transitional mixtures and the kaolinite-controlled mixture compressibility.

Coarse sand grains form a stiff granular skeleton in mixtures with low $F_k \leq 25\%$ (refer to fabric sketches, Fig. 2). The mass fraction of kaolinite $F_k$ compacted at
Table 1. Index properties of sand and kaolinite

<table>
<thead>
<tr>
<th>Property</th>
<th>Silica sand (Jeddha, KSA)</th>
<th>Kaolinite (Gordon, USA)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Size range</td>
<td>76–420 μm</td>
<td>100% finer than</td>
</tr>
<tr>
<td>Specific gravity</td>
<td>$G_s = 2.63$</td>
<td>$G_s = 2.67$</td>
</tr>
<tr>
<td>Maximum void ratio</td>
<td>$e_{\text{max}} = 0.81$</td>
<td>$S_z = 33 \text{ m}^2/\text{g}$</td>
</tr>
<tr>
<td>Minimum void ratio</td>
<td>$e_{\text{min}} = 0.45$</td>
<td>Liquid limits*</td>
</tr>
<tr>
<td>Roundness</td>
<td>0.5</td>
<td>Plastic limit</td>
</tr>
<tr>
<td>Coefficient of uniformity</td>
<td>$C_u = 10$</td>
<td>USCS</td>
</tr>
</tbody>
</table>

†I–I: intermediate plasticity and intermediate sensitivity to pore fluid chemistry. For the new fines classification refers to Jang & Santamarina (2017).

Suction
The SWRC of all 11 mixtures are determined using a dew point hygrometer device (WP4C PotentiaMeter; Campbell et al., 2007). The gravimetric moisture and suction data were gathered during drying. Water potential readings started in wet specimens at a water content slightly lower than the liquid limit. Short drying times were used for the wet samples with suction values <0.1 MPa in order to obtain several measurements. Thereafter, samples were dried in air for ~1 h and equilibrated for >24 h before every reading.

Figure 3 displays the total suction plotted against gravimetric water content for each mixture. A point near the air entry value (AEV) was obtained in all tests. Trends resemble the gap-graded grain size distribution curves as noted in previous studies (rotated by 90°, see Perera et al., 2005). The SWRC signatures exhibit marked differences among specimens; in particular, transitional mixtures exhibit a dual-porosity response (Stoicescu et al., 1996). Single-porosity, kaolinite-dominant signatures are observed for $F_k \geq 25\%$. The trend characteristics are compared in Fig. 4.

- The suction near air entry and at almost-dry conditions ($w = 2\%$) increase with kaolinite content even at very low $F_k$ values (Fig. 4(a)). These trends highlight the controlling effect of small intergranular pores on suction.
- The gravimetric water loss between 100 and 1000 kPa increases as the kaolinite fraction increases (Fig. 4(b)), in agreement with the compressibility trends in Fig. 2 and suction potential in Fig. 4(a). The least water loss takes place near $F_k \approx 20\%$ as intergranular pores in the sand skeleton are filled with kaolinite particles rather than water.

DESICCATION TESTS
Specimen preparation and test procedure
The homogeneously mixed dry mixtures were wetted until a smooth paste was obtained at a water content ~30% higher than the liquid limit. Then, the pastes were evenly laid to fill flat trays (300 mm × 300 mm × 20 mm) to emphasise horizontal shrinkage and desiccation crack formation. Trays were kept in an environmental chamber at RH = 40% and $T = 35\,^\circ\text{C}$.

Weight measurements and photographic images taken at regular intervals document the evolution of the specimens.

Gravimetric data
The evaporation rate in terms of gravimetric water content $Δw/Δt \approx 4 \pm 0.3$ was similar in all specimens for the first few hours. The arrows superimposed on evaporation trends in Fig. 5 mark the onset of crack formation. Specimens with low $F_k \leq 15\%$ did not develop cracks.
The authors used the cone penetration method to determine the liquid limit \( w_L \) for all mixtures. The liquid limit of 100% sand is estimated as the water content in saturated sand at the maximum void ratio \( e_{\text{max}} \). Figure 6 compares the liquid limit \( w_L \), gravimetric water content at fracture initiation \( w_{\text{frac}} \) and water content at air entry \( w_{\text{AE}} \) obtained from the water retention curves; the following trends are seen.

- The gravimetric water contents at fracture initiation \( w_{\text{frac}} \) follow closely the AEVs \( w_{\text{AE}} \) obtained from the water retention curves. Both values are lower than the corresponding liquid limit \( w_L \) (note: as a corollary, soils are saturated at the liquid limit).
- Consequently, desiccation cracks form in saturated soft sediments when the immiscible air phase is suction driven to invade the water-saturated sediment (Shin & Santamarina, 2011b).
- The liquid limit is not linear with the mass fraction of kaolinite, in general agreement with mixture data presented in Sivapullaiah & Sridharan (1985). However, the data in Fig. 6 show that the minimum liquid limit – determined with the cone method – takes place at \( F_K \approx 25\% \). The higher liquid limits for sand-controlled mixtures point to the pore-filling role of kaolinite at low fines fraction \( F_K < 25\% \), refer to the fabric sketches in Fig. 2. Eventually, kaolinite controls the mixture plasticity for \( F_K > 25\% \).

Trends group mixtures into three zones: coarse-controlled with minimal volume contraction and undetected cracks,
intermediate transitional mixtures and fines controlled with well-defined fracture patterns. Once again, the RSCS boundaries are in agreement with transitions in capillary phenomena that are summarised in Fig. 6.

Desiccation and cracks
Time-lapse photography and digital image analysis provided detailed spatial data to assess crack initiation and propagation (similar to the methodology used in Lu & Kaya, 2013). Vertical contraction changes to lateral contraction at the onset of fracture formation (similar to observations in Shin & Santamarina, 2011b). Edge separation.cracks appear in mixtures with kaolinite fractions $F_K = 20$ and 25%; both edge and internal cracks form in all other mixtures with higher clay content.

Figure 7 presents thresholded photographs of all the specimens that experienced edge separation and internal cracks. Crack patterns exhibit the standard $T$ and $Y$ intersections that reflect the evolving effective stresses and formation history.

The crack intensity factor (CIF) relates the area of edge and internal cracks to the total area of the tray (Miller et al., 1998).
The approximation for the linear contractile strain 
\[ \varepsilon_x \approx \frac{CIF}{2} \] applies to small strains. There is a pronounced 
increase in contractile strain when the kaolinite mass 
fraction exceeds \[ F_k \geq 20\% \] (Fig. 7).

**Suction–contraction**

A Bishop-like formulation allows for a first-order estimate of 
the strain the sediment would experience in the horizontal 
direction as the suction increases from \[ \Psi = AEV \] (near-
fraction initiation–Bishop’s \[ \lambda_{AE} \approx 1.0 \]) to a value of suction 
\[ \Psi_{\text{AE}} \text{ measured at near-dry conditions } w = 2\% \]

\[ \varepsilon_{\text{est}} = \frac{C_c}{1 + e_{\text{AE}}} \log \frac{\lambda_{AE} \Psi_{\text{AE}}}{\Psi_{\text{AE}}} \] (3)

The transverse compressibility is in the order of \( C_c \) values 
(Fig. 2), and the gravimetric water content at air entry 
defines the void ratio \( e_{\text{AE}} \). The measured \( e_x \) and estimated strains \( \varepsilon_{\text{est}} \) match for mixtures with high kaolinite content 
when the Bishop parameter is \( \lambda_{2\%} \approx 0.021 \) for near-dry 
conditions \( w = 2\% \) (Fig. 7 – \( \lambda_{2\%} \) is assumed constant for 
all mixtures). The low \( \lambda_{2\%} \) value confirms a high degree of 
air invasion into sediment blocks between desiccation 
cracks. This analysis would suggest that early air invasion 
results in low \( \lambda \) values and diminishes the effect of suction on 
contraction.

Base friction hinders free contraction and promotes more 
closely spaced desiccation cracks. In fact, preliminary 
experiments that involved mixtures placed on Teflon-coated trays 
resulted in edge separation in all mixtures (also note that the 
predicted strains are larger than the measured strains \( \varepsilon_{\text{est}} > \varepsilon_x \) 
for all specimens with a low kaolinite content in Fig. 7). In 
natural systems, the layer thickness and its lateral extent 
affect the development of desiccation cracks. For example,
giant desiccation cracks have been observed in large valleys filled with sandy sediments with some fines – that is, stiff skeleton with low $F_i$ values. Small-scale laboratory experiments are inherently unable to reproduce desiccation crack formation in such sediments. Analytical and empirical equations predict that both suction $\psi$ and compressibility $C_s$ increase with specific surface $S_s$.

From Laplace’s equation – at entry

$$\psi = \frac{2T \rho}{c} S_s$$

From $C_s$–$\psi$ and $\psi$–$S_s$ correlations

$$C_s = 0.02 + 0.005S_s$$

where $T$ is the surface tension, $\rho$ is the mineral mass density and the pore radius is estimated as $\ell(pS_s)$ for parallel platy particles. Therefore, soils that can mobilise higher suction tend to be more compressible; this global trend prevails even in gap-graded mixtures such as those tested in this study. Suction and compressibility combine to cause the large horizontal strains associated with desiccation cracks (equation (3)).

CONCLUSIONS

Saturated soils solidify and stiffen as water evaporates. Eventually, suction causes air invasion. The gravimetric water content at air entry in SWRCs is about the same as the water content at fracture initiation in desiccation tests; both gravimetric water contents are lower than the liquid limit. Therefore, desiccation cracks open-mode discontinuities driven by air invasion into soft sediments.

Desiccation crack formation is a coupled suction–contraction process. Overall, suction and compressibility increase with the soil-specific surface and have a compounded effect on the development of desiccation cracks. In gap-graded sand–clay mixtures, compressibility trends define three marked zones: sand-controlled, transitional and clay-controlled mixture compressibility. However, suction at selected saturation conditions increases with clay content even at very low clay fractions.

Boundary conditions are intimately involved in fracture formation. Both the layer thickness and its lateral extent affect the development of desiccation cracks. Small-scale laboratory experiments are inherently unable to reproduce field-observed desiccation cracks in clayey sands with sand-controlled skeletal stiffness, even when the clay fraction can sustain high suction.

The recently proposed RSCS properly anticipates compressibility trends and the transitions in capillary phenomena observed in this study – that is, between 15 and 35% fines content for sand–kaolinite mixtures.

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