Low SNR Capacity of FSO Links over Gamma-Gamma Atmospheric Turbulence Channels
Abstract—In this paper, we study the ergodic capacity of free space optical communication systems over Gamma-Gamma atmospheric turbulence fading channels with perfect channel state information at both the transmitter and the receiver. In our framework, we mainly focus on the low signal-to-noise ratio range and show that the ergodic capacity scales proportionally to $\text{SNR} \log(1/\text{SNR})$. We show also that one-bit CSI feedback at the transmitter is enough to achieve this capacity using an on-off power control scheme.

Index Terms—FSO, Gamma-Gamma distribution, ergodic capacity, water filling, On-Off power control, low SNR.

I. INTRODUCTION

Free-space optical (FSO) communication systems provide high data rates over short distances and are cost effective. FSO communications may be preferred to its counterpart radio frequency (RF) communications in the sense that they are more secure and alleviate the undesirable frequency spectrum segmentation. Moreover, FSO communications have been proposed in order to complement RF communications in hybrid (RF-FSO) systems. However, the performance of the optical channels depends on the external atmospheric conditions caused by the variations of the refractive index. Indeed, the performance of the laser beam can be easily diminished by turbulence induced scintillation as it propagates in the atmosphere [1]–[5]. In order to evaluate the impact of atmospheric turbulence, various models have been proposed to describe the optical wireless channel statistical characteristics. While the log-normal distribution has been found to be the most suitable for the weak-to-moderate turbulence channels, the Gamma-Gamma (GG) distribution has been found to be the most suitable modeling of the optical channels for moderate- to-strong turbulence channels [1]–[11]. This distribution is produced from the product of two Gamma random variables and is also known as the generalized K distribution.

The ergodic capacity is an important figure giving an important benchmark on the data rate that can be supported by the communication link. In RF communications, much interest has been conducted in studying the performance limits of any communication link at low power regime (or equivalently low signal-to-noise ratio (SNR)) [12]–[14]. In [15], upper and lower bounds on the capacity are derived where the channel has a nonnegative input corrupted by an additive white Gaussian noise and constrained to both an average and a peak power constraint. The authors show that the ratio between the upper and lower bounds tends to one when the average power tends to zero. They also show that when only an average power constraint is adopted, the ratio tends to $2\sqrt{2}$ as the average power tends to zero. However, to the best of our knowledge, no explicit characterization of the capacity where the input is constrained to an average power constraint in the low power regime was investigated in FSO communications. Motivated by this, we provide in this letter a thorough analysis of the ergodic capacity of the FSO channel subject to atmospheric turbulence and using optimal power and rate adaptation (OPRA) in the low SNR regime.

A closed form expression for the average capacity using optimal rate adaptation (ORA) is derived for the GG atmospheric turbulence in [7]–[9]. A closed form expression of the average capacity for the Log-Normal atmospheric turbulence has been also derived in [7], [9]. A closed form expression for the outage probability is derived for the cases when the scintillation follows a log-normal probability distribution over weak atmospheric turbulence channels and GG probability distribution over moderate-to-strong atmospheric turbulence channels in [7], [10]. In [6], Gappmair has derived closed-form expression of the average capacity of FSO channels in turbulent atmosphere for adaptation policies other than ORA, such as the OPRA, channel inversion with fixed rate (CIFR) and truncated channel inversion with fixed rate (TIFR). In [11], a new upper bound on the capacity of power and bandwidth constrained optical wireless links over GG atmospheric turbulence channels is presented, when on-off keying (OOK) formats are used. However, most of the proposed closed-form expressions in the literature do not give much insight because of the presence of the Meijer’s G-function. Moreover, the capacity for the OPRA policy in [6] depends on the optimized cut-off SNR that itself depends on the average SNR and it is not clear how the capacity depends on the SNR. In order to better understand this dependence, we consider the asymptotic behavior of the capacity and characterize its dependence in the low SNR regime assuming ORA and when the optimized cut-off SNR (or the Lagrange multiplier in our framework) is obtained using a water-filling policy for power adaptation. We also propose an on-off scheme that achieves the capacity at asymptotically low SNR regime and that only requires one bit feedback from the receiver side.

The remainder of this paper is organized as follows. Section II describes the system model. Our new low SNR capacity results with perfect channel state information (CSI) at both the receiver and the transmitter are derived in Section III. Finally, some selected numerical results and concluding remarks are discussed in Sections IV and V, respectively.

II. SYSTEM AND CHANNEL MODELS

We consider a point-to-point FSO communication system using intensity modulation/direct detection. The laser beam propagates through a direct path in the turbulence channel corrupted at the receiver by an additive white Gaussian noise (AWGN). The channel model can be given by [2], [7], [9]

$$y = sx + n = \eta Ix + n,$$

where $y$ is the output of the channel, $x$ is the input of the channel, $s = \eta I$ is the instantaneous channel gain, where $I$ is the normalized irradiance and $\eta$ is the effective photo-current conversion ratio of the receiver, and $n$ is the AWGN with a zero mean and a variance $N_0$ normalized to 1. We suppose that both the receiver and the transmitter have full knowledge of
the channel gain. The source is subject to an average electrical power constraint $P_{av}$, where $E[\cdot]$ is denoting the expectation operator, and $P_{avg}$ may also be seen as the average transmit SNR as we have a normalized noise. Note that, although the average optical power is limited in FSO context for eye and skin safety, in the most practical optical sources, it is the average power constraint that is more restrictive than the peak power constraint [4, 6, 11, 16–20]. Moreover, our system is subject to only an average electrical power constraint, and not to an average optical power constraint. The average power of the optical signal and the average power of the electrical current at the transmitter side are shown to be connected in [4], [20] and the spectral efficiencies obtained by the average electrical power constraint is lower bounded by the spectral efficiencies obtained by the average optical power constraint since an average optical power constraint implies an average electrical constraint. In our case, for a positive Gaussian input distribution with variance $\sigma^2$, it is easy to show that $E[x] < P_{opt}$ is necessary and sufficient condition for satisfying $E[x^2] < P_{avg}$, since $\sigma^2 = E[x^2] - E[x]^2$ provided that $P_{avg} = \sigma^2 + P_{opt}$ [4]. We mainly focus on asymptotically low SNR, i.e., $P_{avg} \to 0$.

For moderate-to-strong turbulence, the irradiance is modeled by a GG distribution [4], [11] whose probability density function (PDF) is given by

$$f_a(I) = \frac{2(ab)^{\nu a}}{\Gamma(a)\Gamma(b)} I^{\nu a - 1} K_{a-b}(2\sqrt{ab}I),$$

where $K_{a-b}$ is the modified Bessel function of second kind and of order $\nu$, $\Gamma(.)$ is the Gamma function and $a \geq 0$ and $b \geq 0$ are the distribution shaping parameters that can be expressed as

$$a = \left[ \exp \left( \frac{0.49\ \delta^2}{(1 + 0.18\ d^2 + 0.56\ \delta^{12/5})^{5/6}} - 1 \right) \right]^{-1}$$

and

$$b = \left[ \exp \left( \frac{0.51\ \delta^2}{(1 + 0.9\ d^2 + 0.62\ \delta^{12/5})^{5/6}} - 1 \right) \right]^{-1}$$

where $\delta^2 = 1.23C_n^2/16L^{1/6}$ is the Rytov variance and $d = \sqrt{\mathbf{K}}/\mathbf{L}$ is the optical wave number, $L$ is the length of the optical link, $D$ is the receiver’s aperture diameter and $C_n^2$ is the altitude turbulence strength and varying from $10^{-17}$ m$^{-2/3}$ for weak turbulence to $10^{-13}$ m$^{-2/3}$ for strong turbulence depending on the atmospheric turbulence conditions. The instantaneous value of the equivalent channel gain according to (1) is defined as $\gamma = \frac{(\eta) I^2}{N_0} = \eta^2 I^2$.

This definition of SNR is governed by an average electrical power constraint and is similar to the one in [4]–[9], [21]–[23] for studying the performance of FSO communication systems. This definition is somehow different from the definition that is usually adopted in FSO systems, which is basically governed by an average power constraint. This definition of SNR governed by an average electrical power constraint emphasizes the role of the receiver which operates in the thermal noise-dominated scenario, and whose performance depends on the average power of the electrical current, obtained by the conversion from the optical signal. Moreover, this definition of SNR proper to RF channels also allows us to fairly compare the capacity gain due to CSI at the transmitter (CSI-T) in FSO links compared to RF links. The PDF of $\gamma$ can then be obtained from (2) by a transformation of the random variable I [7], [9]

$$f_\gamma(\gamma) = \frac{(ab)^{\nu a}}{\Gamma(a)\Gamma(b)} \frac{\gamma^{\nu a - 1}}{\Omega^{\nu a - \frac{1}{2}}} K_{a-b} \left( \frac{2\sqrt{ab}}{\sqrt{\Omega}} \right).$$

where the average power of the equivalent channel gain is equal to $\Omega = (\eta I)^2 = \eta^2 [9]$. The instantaneous optimal power $P(\gamma)$ is given by the water-filling policy [24]

$$P(\gamma) = \left[ \frac{1}{\lambda(SNR)} - \frac{1}{\gamma} \right]^+,$$

where $\lambda(SNR)$ is the Lagrange multiplier obtained by satisfying the average power constraint with equality:

$$P_{avg} = SNR = E_{\gamma} [P(\gamma)].$$

At this point, let us define the function $G(x)$ over $(0, \infty)$ as

$$G(x) = E_{\gamma} \left[ \left[ 1 - \frac{1}{x} \right]^+ \right],$$

where $G(.)$ is continuous, positive definite and strictly monotonically decreasing [14, Lemma 1] and it satisfies $G(\lambda(SNR)) = P_{avg} = SNR$. Next, we focus on asymptotically low SNR regime, i.e., $P_{avg} \to 0$, in which it is useful to define $f(x) \approx g(x)$ if and only if $\lim_{x \to 0} f(x) = 0$.

III. LOW-SNR CAPACITY WITH PERFECT CSI-T

A. Capacity Results

The ergodic capacity is obtained by averaging log(1+$\gamma$) over $\gamma$ and is given by

$$C(\lambda(SNR)) = \int_0^{\infty} \left[ \frac{1}{\lambda(SNR)} - \frac{1}{x} \right]^+ f_\gamma(x) \, dx = \int_{\lambda(SNR)}^{\infty} \log \left( \frac{x}{\lambda(SNR)} \right) f_\gamma(x) \, dx.$$ (9)

The low-SNR capacity of the FSO channel is given in Theorem 1.

Theorem 1: For a FSO communication channel described by (1), with perfect CSI at both the transmitter and the receiver, the low-SNR capacity is given by

$$C \approx \frac{\Omega \ m^4 \ SNR}{16(ab)^2} W_4 \left( \frac{2\sqrt{ab}}{\Omega^{1/2}} (\tau \ SNR)^{\frac{\nu a}{2}} \right),$$

if $m > 0$,

$$C \approx \frac{\Omega \ m^4 \ SNR}{16(ab)^2} W_4 \left( \frac{2\sqrt{ab}}{\Omega^{1/2}} (\tau \ SNR)^{\frac{\nu a}{2}} \right),$$

if $m = 0$,

$$C \approx \frac{\Omega \ m^4 \ SNR}{16(ab)^2} W_4 \left( \frac{2\sqrt{ab}}{\Omega^{1/2}} (\tau \ SNR)^{\frac{\nu a}{2}} \right),$$

if $m < 0$.

(11)

where $m = \frac{13}{2} - (a + b)$, $\tau = \frac{\Gamma(a)\Gamma(b)\Omega^{\frac{\nu a}{2} - \frac{1}{4}}}{2\sqrt{\pi} \Gamma(ab) \Omega^{\frac{\nu a}{2} - \frac{3}{4}}}$, and $W_0(.)$ and $W_{-1}(.)$ are the principal branch and the lower branch of the Lambert W-function, respectively.

Proof: First, recall $G(.)$ is a strictly monotonically decreasing function [14, Lemma 1], i.e. as $SNR \to 0, \lambda \to \infty$. Thus, we can use the series expansion of the modified Bessel function of second kind at infinity [25]

$$K_a(x) \approx \sqrt{\frac{\pi}{2x}} e^{-x} \left( \sum_{k=0}^{\nu a} \left( \frac{1}{2x} \right)^k \frac{\Gamma(v + k - \frac{1}{2})}{\Gamma(v - k - \frac{1}{2})} \right),$$ (12)

Then, we can substitute (12) in (9) to obtain

$$C(\lambda(SNR)) \approx \frac{\sqrt{\pi}}{2(\gamma \Gamma(b))} \frac{ab^{-\nu a - \frac{1}{2}}}{\Omega^{\nu a - \frac{1}{2}}} \int_{\lambda}^{\infty} \log \left( \frac{x}{\lambda} \right)^{\frac{\nu a}{2} - \frac{1}{4}} e^{-2\sqrt{ab} \sqrt{\pi} x} \, dx,$$

$$\approx \frac{\sqrt{\pi}}{2(\gamma \Gamma(b))} \frac{ab^{-\nu a - \frac{1}{2}}}{\Omega^{\nu a - \frac{1}{2}}} I_4(\lambda),$$ (13)
with
\[ I_c(\alpha) \approx \frac{1}{\sqrt{\pi}} \frac{\Gamma((a+b)\Omega^{2/3})}{\Gamma(2,\frac{\Omega}{2})} \left[ 2 \sqrt{ab} \left( \frac{\Omega}{2} \right)^{3/2} e^{-2 \sqrt{ab} \sqrt{\Omega}} \right], \]
with \( G_{\lambda,\mu}^{\mu,\mu}(.,.) \) describes the Meijer’s G-function [25]. Using series expansion of the Meijer’s G-function at infinity [25], we obtain
\[ C(\lambda(SNR)) \approx \frac{1}{\tau} \frac{\alpha^{\frac{a+b}{2} - 1}}{\Omega^{\frac{a+b}{2} + 1}} \int_0^1 \left( 1 - \frac{x}{\lambda} \right)^{\frac{a+b}{2} - 1} e^{-2 \sqrt{ab} \sqrt{\Omega} x} \, dx, \] (14)
with \( \tau = \frac{\Gamma(a)\Gamma(b)\Omega^{2/3-1}}{2 \sqrt{\pi}(ab)^{1/2}} \). On the other hand, using (12) in (8) for \( \lambda = \lambda(SNR) \), we obtain
\[ SNR \approx \frac{\sqrt{\pi}}{2\Gamma(a)\Gamma(b)} \frac{(ab)^{2/3}}{\Omega^{2/3 + 1}} \int_0^\infty \left( \frac{1}{\lambda} - \frac{1}{x} \right) x^{ab - 1} e^{-2 \sqrt{ab} \sqrt{\Omega} x} \, dx, \]
\[ \approx \frac{\sqrt{\pi}}{2\Gamma(a)\Gamma(b)} \frac{(ab)^{2/3}}{\Omega^{2/3 + 1}} \left[ I_1(\lambda) - I_2(\lambda) \right], \] (15)
where
\[ \begin{aligned}
I_1(\lambda) &= \frac{4\Gamma(a+b)}{(2\sqrt{\pi})\ln\lambda} \int_0^\infty \left( 1 - \frac{1}{\lambda} \right) \frac{1}{x^{a+b} - 1} 2 \sqrt{ab} \sqrt{\Omega} x, \\
I_2(\lambda) &= \frac{4\Gamma(a+b)}{(2\sqrt{\pi})\ln\lambda} \int_0^\infty \left( 1 - \frac{1}{\lambda} \right) \frac{1}{x^{a+b} - 1} 2 \sqrt{ab} \sqrt{\Omega} x,
\end{aligned} \] (16)
where \( \Gamma(.,.) \) is the incomplete Gamma function. Then using the series expansion of \( \Gamma(.,.) \) function at infinity [25] in (15) yields
\[ SNR \approx \frac{1}{\tau} \frac{\alpha^{\frac{a+b}{2} - 1}}{\Omega^{\frac{a+b}{2} + 1}} \int_0^\infty \left( 1 - \frac{1}{x} \right)^{\frac{a+b}{2} - 1} e^{-2 \sqrt{ab} \sqrt{\Omega} x} \, dx, \] (17)
From (14) and (17), we can verify that \( C(\lambda(SNR)) = SNR \lambda(SNR) \). In order to characterize how the capacity scales as a function of the SNR, let us first solve (17) to characterize how the Lagrangian multiplier \( \lambda(SNR) \) varies in function of the SNR. Note that (17) can be put in the form \( y = xe^x \) and its solution can be expressed as a function of the principal and the lower branches of the Lambert W-function depending on the value of \( m = 13/2 - (a + b) \).

- If \( m < 0 \), a solution of (17) can be expressed as function of the lower branch of the Lambert W-function given that \( 2 \frac{\sqrt{ab}}{m} \left( \frac{\lambda}{\Omega} \right)^{1/4} < 0 \) and it is expressed as
\[ \lambda(SNR) \approx \left[ \frac{m \Omega^{3/2}}{2 \sqrt{ab}} W_{-1} \left( \frac{2 \sqrt{ab}}{m \Omega^{3/2}} \left( \tau SNR \right)^{2/3} \right) \right]. \] (18)

Although the Lambert W-function is a built-in function in standard software, we express the capacity in terms of the popular \( \log(.) \) function using an infinite ladder self-mapping technique given in [26]. The solution to the equation \( y = xe^x \) with \( x > 1 \) or \( y > e \) can be expressed as \( x = L_+(y) \), with \( L_+(y) = -\log \left( -\log \left( \frac{\log(-y)}{y} \right) \right) \). For instance, the first infinite functional series is \( \log(y) \) and hence we have
\[ \lambda(SNR) \approx \frac{m \Omega^{3/2}}{16(ab)^2} \log^4 \left( \frac{2\sqrt{ab}}{m \Omega^{3/2}} \left( \tau SNR \right)^{2/3} \right), \] (19)
We know that \( \lim_{y \to 0} \frac{\log(-\beta y)}{\log(-y)} = 1 \), for any \( \beta > 0 \) and \( y < 0 \) and hence the result in Theorem 1.

- If \( m > 0 \), a solution of (17) can be expressed in function of the principal branch of the Lambert W-function given that \( 2 \frac{\sqrt{ab}}{m} \left( \frac{\lambda}{\Omega} \right)^{1/4} > 0 \) and it is expressed as
\[ \lambda(SNR) \approx \left[ \frac{m \Omega^{3/2}}{2 \sqrt{ab}} W_0 \left( \frac{2 \sqrt{ab}}{m \Omega^{3/2}} \left( \tau SNR \right)^{2/3} \right) \right]. \] (20)

Similar to the previous case, we also express in this case the capacity in terms of the popular \( \log(.) \) function. In this case, the solution to the equation \( y = xe^x \) with \( x < -1 \) or \(-1/e < y < 0 \) can be expressed as \( x = L_-(y) \), with \( L_-(y) = -\log \left( \frac{\log(-y)}{y} \right) \). For instance, the first infinite functional series is \( \log(-y) \) and hence we have
\[ \lambda(SNR) \approx \frac{m \Omega^{3/2}}{16(ab)^2} \log^4 \left( \frac{1}{\tau SNR} \right), \] (23)
where \( \tau \) is equal to \( \Gamma(a)\Gamma(b)\Omega^{2/3} \) when \( m = 0 \).

This completes the proof of Theorem 1.

The asymptotic characterization of the capacity provided in Theorem 1 states that at low SNR, the energy efficiency defined as the ratio of the transmitted energy in Joules per information nats by the noise variance of an FSO communication system is proportional to the inverse of \( \log^4(1/SNR) \), which means that communicating one nat of information over a FSO link undergoing a GG fading channel requires much lower energy compared to an RF link undergoing Nakagami fading where the energy efficiency with perfect CSI-T scales essentially as \( 1/\log(1/SNR) \) [14].

B. On-Off Power Control Is Asymptotically Optimal

In this subsection, we will design a practical scheme in order to asymptotically achieve the capacity using the results gained in Theorem 1. Let us consider an on-off power control that transmits whenever \( \gamma \geq \lambda(SNR) \) and remains silent otherwise. Thus, given the power constraint, the instantaneous power \( P(\gamma) \) is given by
\[ P(\gamma) = \begin{cases} \frac{S_{\text{NR}}}{\log(\gamma_{\text{nr}})}, & \text{if } \gamma \geq \lambda(SNR) \\
0, & \text{otherwise,} \end{cases} \] (24)

The achievable rate in this case is given by
\[ R(SNR) = \mathbb{E}_{\gamma} \left[ \log(1 + P(\gamma)\gamma) \right], \] (25)
\[ \geq \int_{\lambda(SNR)}^{\infty} \log \left( 1 + \frac{\lambda(SNR)S_{\text{NR}}}{\log(\gamma_{\text{nr}})} \right) f_{\gamma}(t) \, dt, \]
\[ = \log \left( 1 + \frac{\lambda(SNR)S_{\text{NR}}}{\log(\gamma_{\text{nr}})} \right) \text{Prob}(\gamma \geq \lambda(SNR)). \] (26)
where \( \text{Prob}(\gamma \geq \lambda(SNR)) \) can be written as
\[
\text{Prob}(\gamma \geq \lambda(SNR)) = \frac{\sqrt{\pi}}{2\Gamma(a)\Gamma(b)} \frac{(ab)^{\frac{a+b-1}{2}}}{\Omega^{\frac{a+b}{2}}} I_1(\lambda),
\]
(27)

\[
\approx \frac{1}{2} \frac{(ab)^{\frac{a+b-1}{2}}}{\Omega^{\frac{a+b}{2}}} e^{-2\sqrt{\pi} \frac{\lambda}{\Omega}},
\]
(28)

Obviously, (28) is obtained from (27) using (16) and the series expansion of \( \Gamma(\ldots) \) function at infinity [25]. Then, we can write
\[
\frac{\lambda(SNR)SNR}{\text{Prob}(\gamma \geq \lambda(SNR))} \approx \frac{2\Omega}{\lambda} \frac{1}{(ab)^{\frac{a+b-1}{2}}},
\]
(29)

which converges to zero when \( \lambda \) goes to infinity. Therefore, given that (29) is a monotonic function of \( \lambda \), we can use the asymptotic approximation \( \log(x + 1) \approx x \) in (26) and deduce that the achievable rate of the on-off scheme is equal to \( \lambda(SNR)SNR \). Hence, 1-bit feedback of CSI-T in each fading realization is enough to achieve the asymptotic capacity. This bit contains the result of the outcome of the comparison between \( \gamma \) and \( \lambda(SNR) \).

IV. NUMERICAL RESULTS

In this section, we present some selected numerical results illustrating the accuracy of our characterization given in Theorem 1. We have plotted the ergodic capacity of an FSO link over GG atmospheric turbulence in nats per information use (npu) with perfect CSI at both the transmitter and the receiver versus the transmit electrical SNR in Figs. 1 and 3, and versus the transmit optical SNR in Fig. 2. The average optical power and the average electrical power are computed given that we have a positive Gaussian input with zero mean and a variance \( \sigma^2 = 10^{-15} \). We consider two different values of the altitude-dependent turbulence strength \( \Gamma \), namely \( 9 \times 10^{-15} \text{m}^{-2/3} \) for moderate turbulence in Figs. 1 and 2, and \( 3 \times 10^{-14} \text{m}^{-2/3} \) for strong turbulence in Fig. 3, respectively. In our analysis, the value of the wavelength has been set to the typically used value, namely 850 nm [5]. The receiver’s aperture diameter and the length of the optical link have been chosen equal to 0.01 m and 1000 m, respectively. The values of \( a \) and \( b \) are then computed using Eqs. (3) and (4). The exact capacity is computed using a numerical root finding algorithm to find the Lagrange multiplier \( \lambda \) that satisfies the average power constraint in (7), and then the exact capacity is computed using (9). The no CSI case corresponds to the case where we have no knowledge of the irradiance at the transmitter. The asymptotic capacity with Lambert W-function and with Log function have been obtained using (10) and (11) in Theorem 1 with full CSI at both the transmitter and the receiver. In order to better understand our characterization with the Lambert W-function in (10), we have also used an infinite ladder self-mapping technique [26].

In Figs. 1 and 2, the values of \( a \) and \( b \) correspond to the case where \( a + b - 13/2 > 0 \). Note from these figures that an accurate characterization of the capacity can be obtained using the good approximation of the Lambert W-function in (10) with 6 iterations of the infinite ladder function \( x_n(y) = L_n(y) \) for \( -1/e < y < 0 \), given that \( x_1(y) = \log(-y) \) and \( x_2(y) = x_1(y) - \log(-x_1(y)), n \geq 2 \). We mention also that although the log characterization is not very accurate in Figs. 1 and 2 in the displayed SNR range, we have verified that as SNR goes to zero, the gap to the exact curve diminishes considerably (not shown here). From the figures 1 and 2, we can see that the spectral efficiencies for an average electrical power constraint is lower bounded by the spectral efficiencies for an average optical power constraint.

In Fig. 3, the values of \( a \) and \( b \) correspond to the case where \( a + b - 13/2 < 0 \). Note from this figure that an accurate characterization of the capacity can again be obtained using the good approximation of the Lambert W-function in (10) using only one iteration of the infinite Ladder function \( x_n(y) = L_n(y) \) for \( e < y < 0 \), given that \( x_1(y) = \log(y) \) and \( x_2(y) = x_1(y) - \log(x_1(y)), n \geq 2 \). In the selected numerical results, we can also characterize the gain of the full CSI-T case versus the no CSI-T case which is proportional to \( \log^3(1/SNR) \) compared to \( \log(1/SNR) \) in RF communications. This gain might be of appealing practical interest for designer of hybrid RF/FSO systems. Furthermore, the on-off achievable rate is also depicted in Figs. 1, 2 and 3, where it can be seen that it is in fact the closest curve to the capacity suggesting that this suboptimal scheme is worth implementing in the low-SNR regime.

V. CONCLUSION

In this paper, we have analyzed the capacity of a FSO wireless communication channel over GG atmospheric turbulence at low SNR and with full CSI at both the transmitter and the receiver. We showed that the capacity scales asymptotically as \( \Omega SNR \text{ log}^3(1/SNR) \). Moreover, an on-off power control scheme has been shown to be asymptotically achieving the capacity using only one-bit CSI feedback at the transmitter. Our framework has not only confirmed the crucial value of CSI-T on the capacity of FSO communications, but has in fact gone beyond to actually state that the gain due to CSI-T essentially equal to \( \log(1/SNR) \) in RF communication, is in fact more substantial in FSO communications.

VI. ACKNOWLEDGEMENTS

Fatma Benkelifa would like to thank Dr. Arsenia Chorti and Prof. H. Vincent Poor for some valuable discussions and exchanges during her visit to Princeton University in June/July 2012.

REFERENCES

Figure 1. Low-SNR capacity in nats per channel use (npcu) versus electrical SNR for moderate turbulence $C_n^+ = 9 \times 10^{-15} m^{-2/3}$ ($a = 6.4900$ and $b = 7.2092$).

Figure 2. Low-SNR capacity in nats per channel use (npcu) versus optical SNR for moderate turbulence $C_n^+ = 9 \times 10^{-15} m^{-2/3}$ ($a = 6.4900$ and $b = 7.2092$).

Figure 3. Low-SNR capacity in nats per channel use (npcu) versus SNR for strong turbulence $C_n^+ = 3 \times 10^{-14} m^{-2/3}$ ($a = 2.7454$ and $b = 3.0543$).